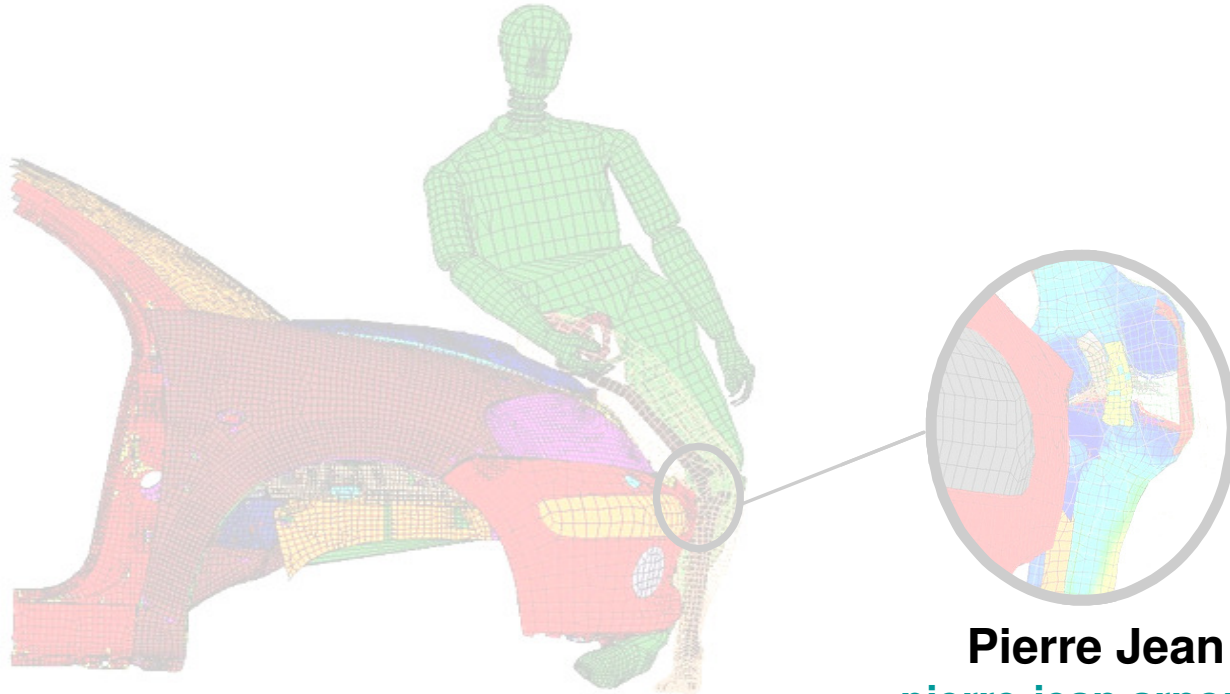


About tissue mechanics and human modeling for trauma understanding



Pierre Jean Arnoux
pierre-jean.arnoux@inrets.fr



Équipe du Laboratoire de Biomécanique Appliquée
UMR T 24, INRETS - UNIVERSITE DE LA MEDITERRANEE



Road Safety in EU : a first order societal issue

- > 40.000 lethal injuries
- ~ 1.700.000 injuries
- First death causation < 45 years old
- Cost : 160 Milliard € : (2% EU PIB)

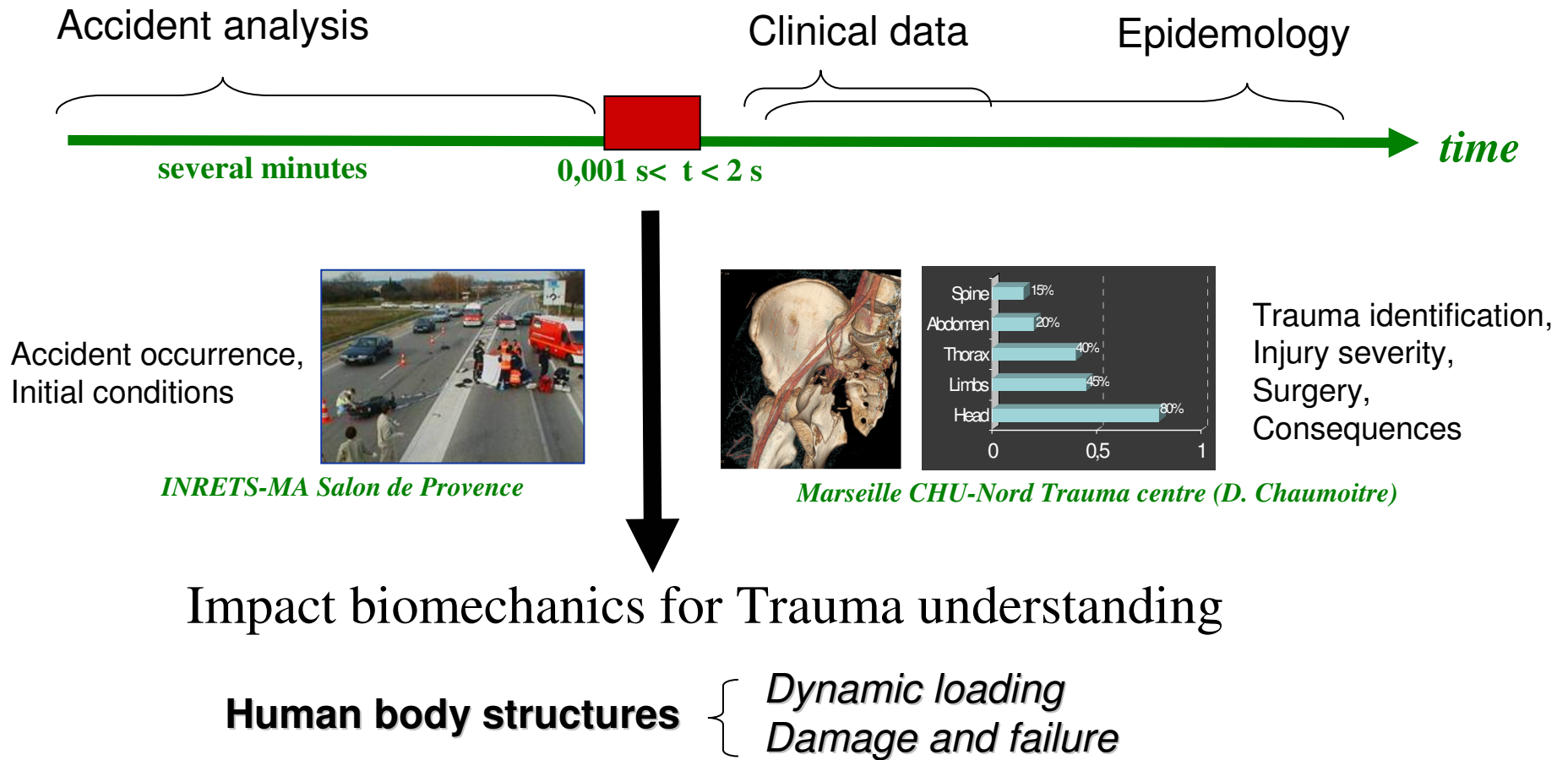
→ A real epidemic

Rapport DG-Tren, commission européenne (2000, 2004, 2008)

An ounce of prevention is worth a pound of cure

« Mieux vaut prévenir que guérir »

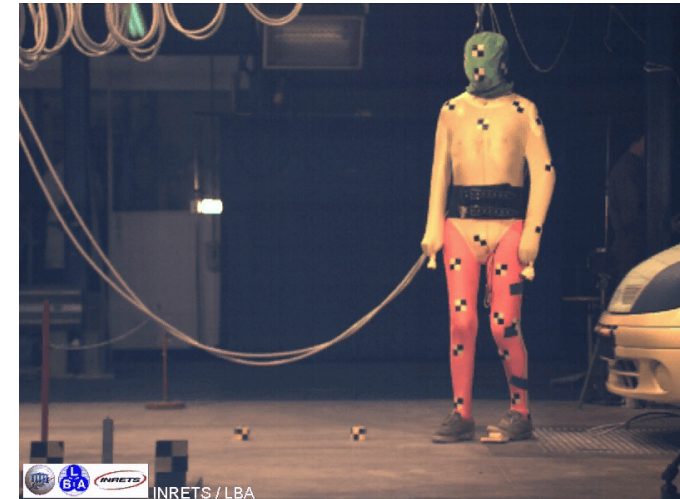
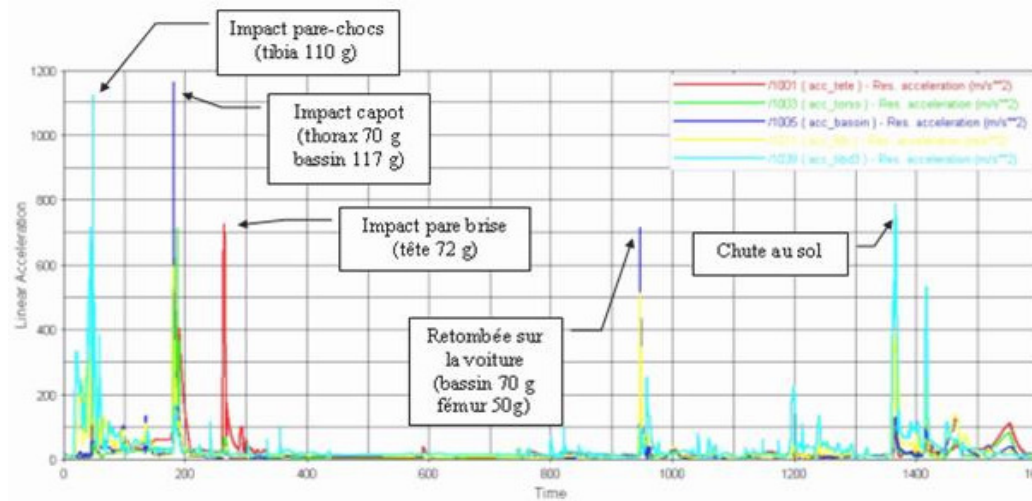
From real crash, trauma understanding...



Experiments & real crash conditions

Pedestrian impact with PMHS

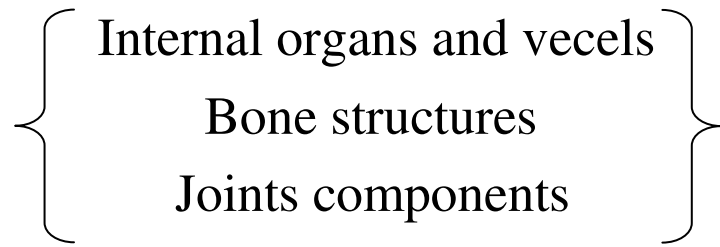
From 1st impact to ground fall



36km/h pedestrian impact (Masson - LBA)

A succession of local impacts with dedicated sub-injuries

Many injuries



Different neighboring structures

Rigidity
Mobility

Which chronology for injuries ?

What about human tolerance ?

Which injury mechanisms ?

Which injury criteria?

Numerical simulation of Human body

A way to investigate virtual trauma

... to improve safety systems

The work plan :

I. Mechanical properties of tissues : *A first step before simulation*

→ **Hard Tissues / Fibrous structures / Soft tissues**

II. On Human body modelling features

→ **Towards explicit detailed FE models**

III. Applications to virtual trauma

→ **Lower limbs, Trunk and Spine**

« après s'être fait la main sur le pied,
l'objectif est de prendre son pied sur le tronc! »
(M. Jean 2005).

I. Mechanical properties of tissues

I. Mechanical properties of living isolated structures

- The framework for tissue identifications

Mechanical identifications performed at structure levels

Dynamical loadings with time scale : from 1 to 10ms

- On difficulties to obtain experiment data

Each tissue is unique : « One shoot for identification ! »

—————→ *Human variability and response corridor*

Tissue conservation and experimental setups

—————→ *Loading conditions relevant with trauma ones*
Needs to design dedicated experiments

Tissue histology —————→ *Complete damage process analysis*



Identify tissues general properties

Model to be implemented in FE analysis

Simplified model to describe the main properties of structures

Ligaments properties identification (1/4)

General properties

From anatomy to histology

Fibrous structure with a main orientation

Crimped structure

Different shapes & dimensions

Contribution to joint stability : traction loading

Mechanical features

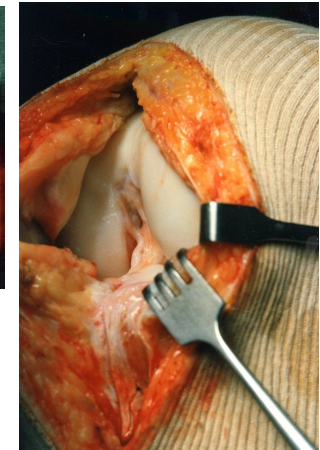
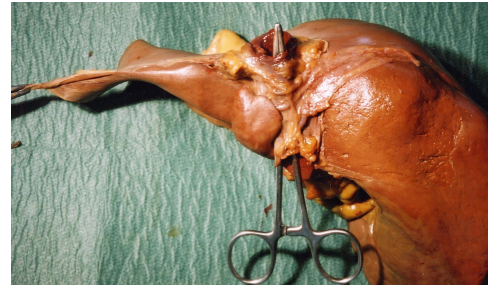
Anisotropy / inhomogeneity / incompressibility

Prestress / An non homogenous strain field

Mechanical behaviour

Viscoelasticity - Non linearity – Large strain

Hyperelasticity



*Ligaments of the liver
And knee ACL injury*

Ligaments properties identifications (2/4)

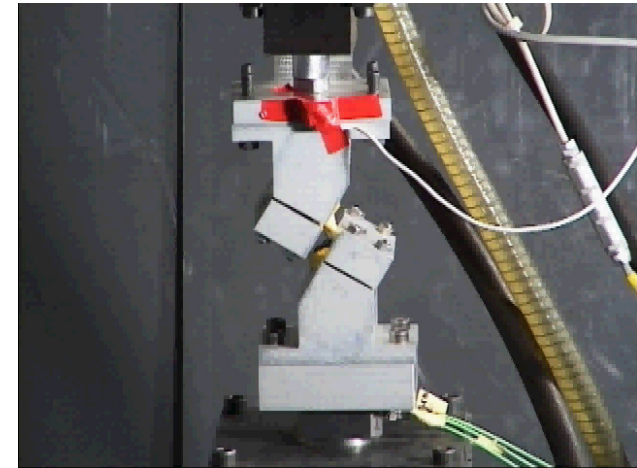
Experimental identification

2m/s traction test on knee ligaments

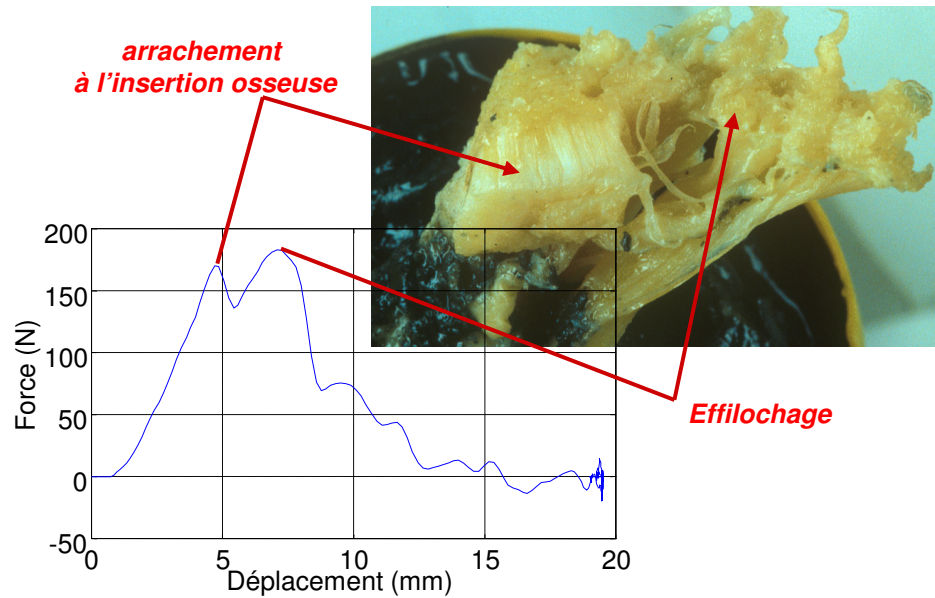
32 ligaments (4 PMHS from 58 to 88 years old) under fibres axes

Damage and failure

- Peeling failure
- Avulsion at bone insertion
- Strong failure reproducibility

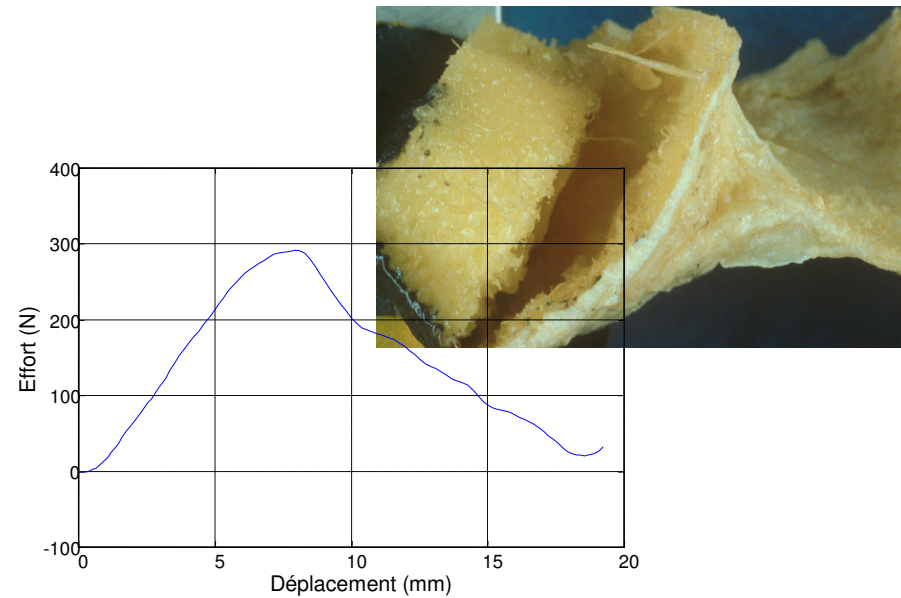


ligaments croisés



Une déformation maximale : 18 à 24%

ligaments latéraux



Une déformation maximale : 22 à 38%

Ligaments properties identifications (3/4)

To viscoelastic model with damage and failure

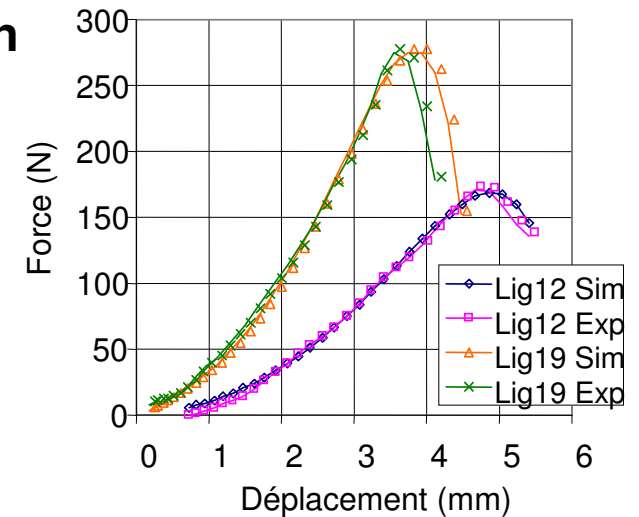
At the macroscopic level: a thermodynamic formulation

$$S = -pC^{-1} + 2(1 - D) \left[\left(\frac{\partial W_e}{\partial I_1} + trC \frac{\partial W_e}{\partial I_2} \right) Id - \frac{\partial W_e}{\partial I_2} C + \frac{\partial W_v}{\partial \dot{C}} \right]$$

$$W_v = \frac{\eta}{4} tr(\dot{C})^2 (I_1 - 3) \quad W_e = \alpha \exp[\beta(I_1 - 3)] + \gamma(I_2 - 3)$$

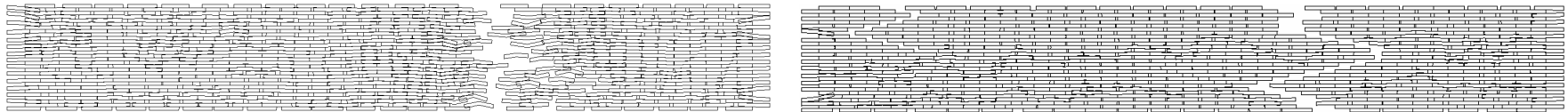
$$\dot{D} = \begin{cases} \frac{n(D + D_0)\dot{\lambda} \left[\alpha\beta \exp\left(\beta\left(\lambda^2 + \frac{2}{\lambda} - 3\right)\right) - \frac{\alpha\beta}{\lambda} \right]}{Q\sqrt{D + D_0}} \\ 0 \end{cases}$$

*Isotropy, homogeneity, incompressibility
Fading memory neglected*



At the microscopic level : failure process evaluation on collagen fibril

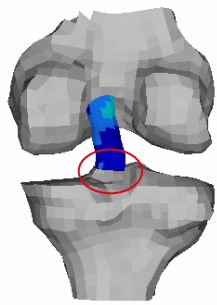
Elastic brick model with Mohr-Coulomb adhesion law : **micro fibril – collagen fibril**



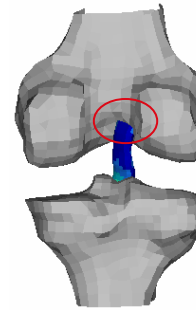
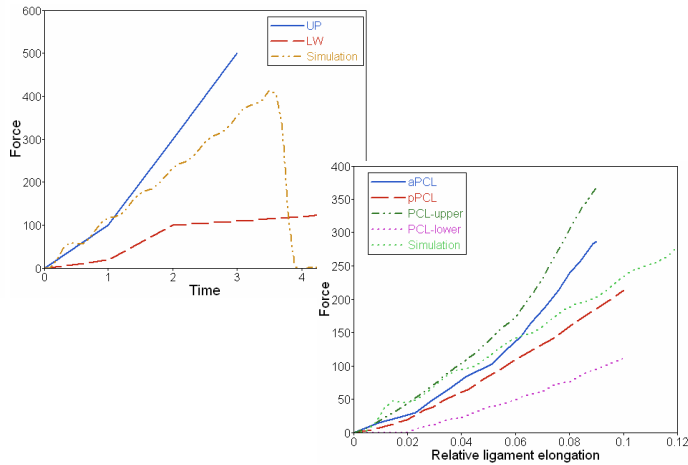
Ligaments properties (4/4)

integration & evaluation on FE model

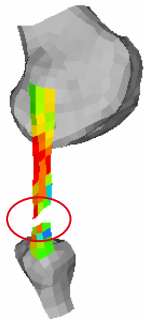
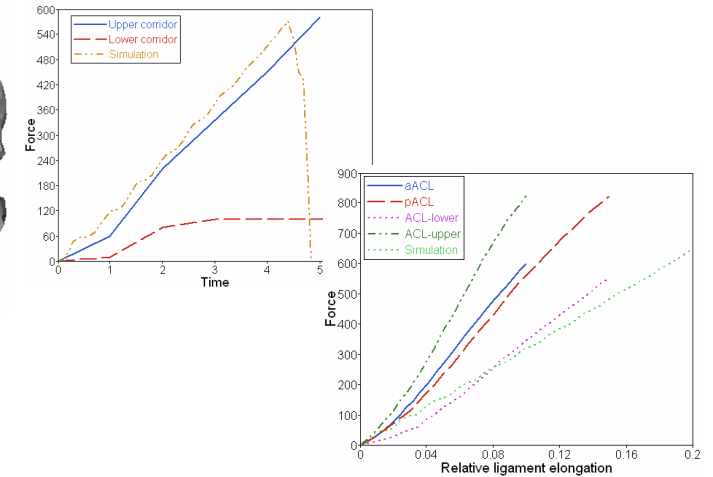
Failure : / Ultimate deformation
Kill element methods



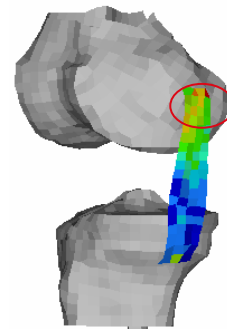
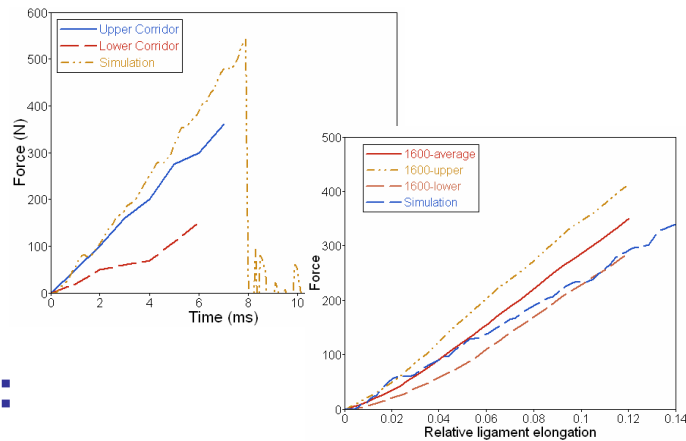
PCL :



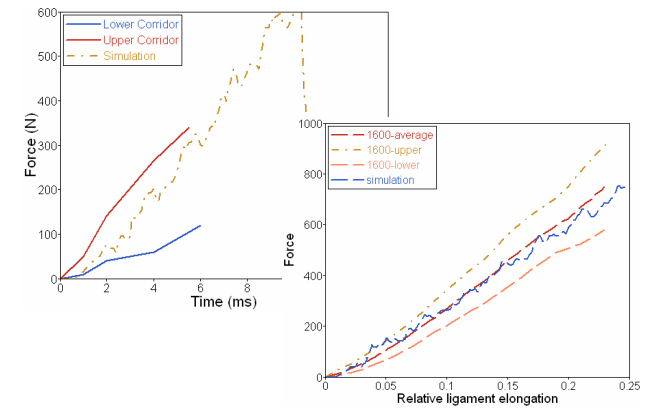
ACL :



LCL :



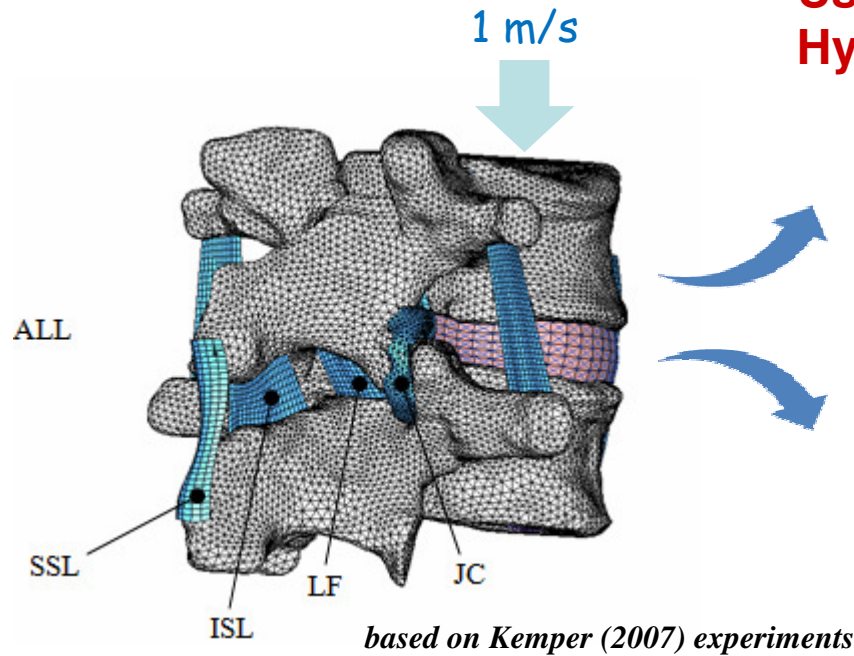
MCL :



Based on previous test (Arnoux 2002) & Dommelen 2005 data

Intervertebral disc properties modelling (1/3)

Using inverse analysis identification
Hyperelastic properties assumption



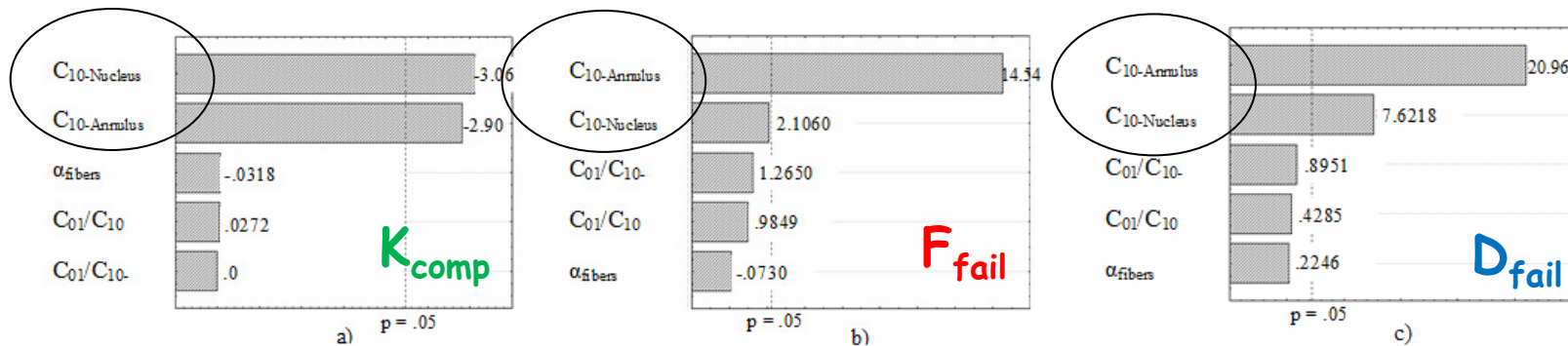
Hyperelastic material formulation (Mooney-Rivlin)

$$W = c_{10}(I_1 - 3) + c_{01}(I_2 - 3) + (J-1)^2/d_1$$

Output :

- Compressive stiffness (K_{comp})
- Failure load (F_{fail})
- Displacement to failure (D_{fail})

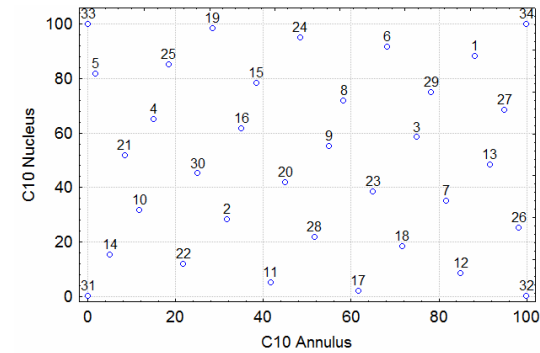
1. Evaluation of influent parameters using exploration and sensitivity analysis (Pareto)



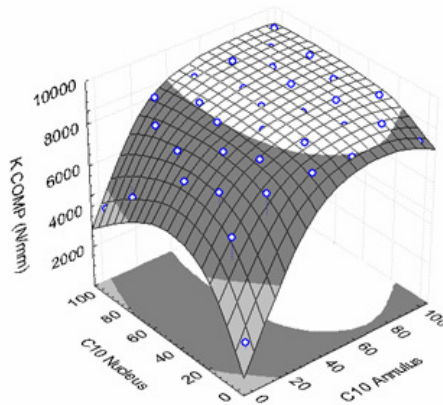
Intervertebral disc properties modelling (2/3)

Selection of 34 sets of C10-Annulus and C10-Nucleus values using a OLH algorithm

→ 34 simulations

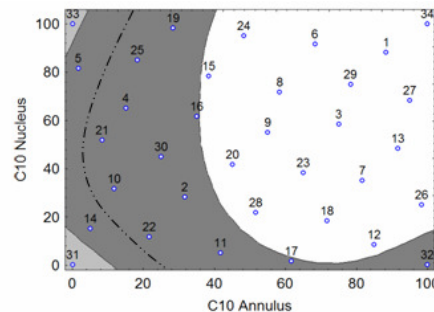


- $K_{COMP} < 4534.1 \text{ N/mm}$
- $4534.1 \text{ N/mm} \leq K_{COMP} \leq 8468.1 \text{ N/mm}$
- $K_{COMP} > 8468.1 \text{ N/mm}$
- $K_{COMP} = 6551.1 \text{ N/mm}$



From surface regression and contour plots

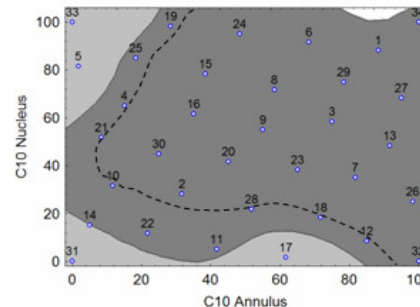
Discriminate and identify admissible set of parameters
According output data



K_{comp}

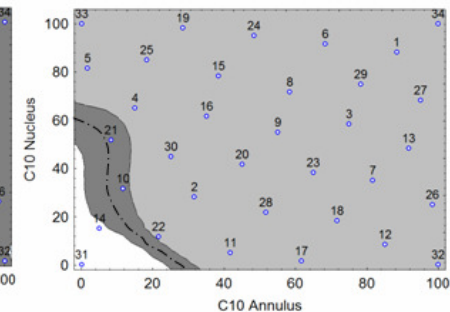
F_{fail}

- $F_{FAIL} < 11203 \text{ N}$
- $11203 \text{ N} \leq F_{FAIL} \leq 13068 \text{ N}$
- $F_{FAIL} > 13068 \text{ N}$
- $F_{FAIL} = 12411 \text{ N}$



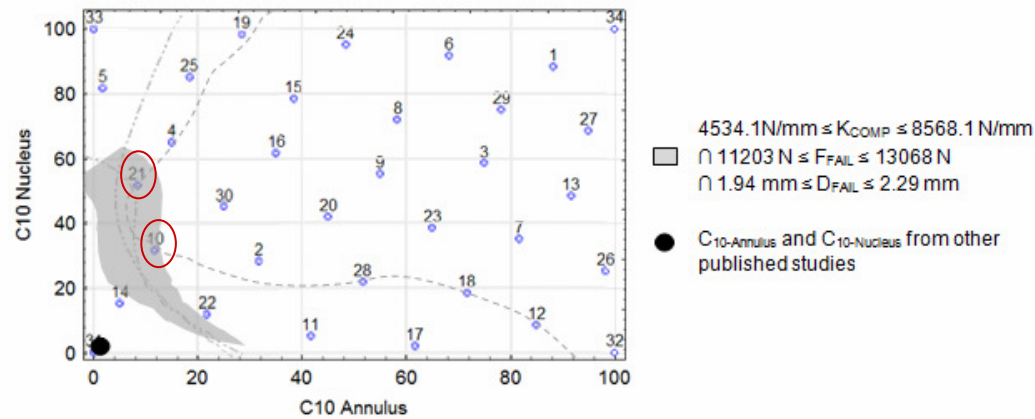
D_{fail}

- $D_{FAIL} < 1.94 \text{ mm}$
- $1.94 \text{ mm} \leq D_{FAIL} \leq 2.29 \text{ mm}$
- $D_{FAIL} > 2.29 \text{ mm}$
- $D_{FAIL} = 2.08 \text{ mm}$

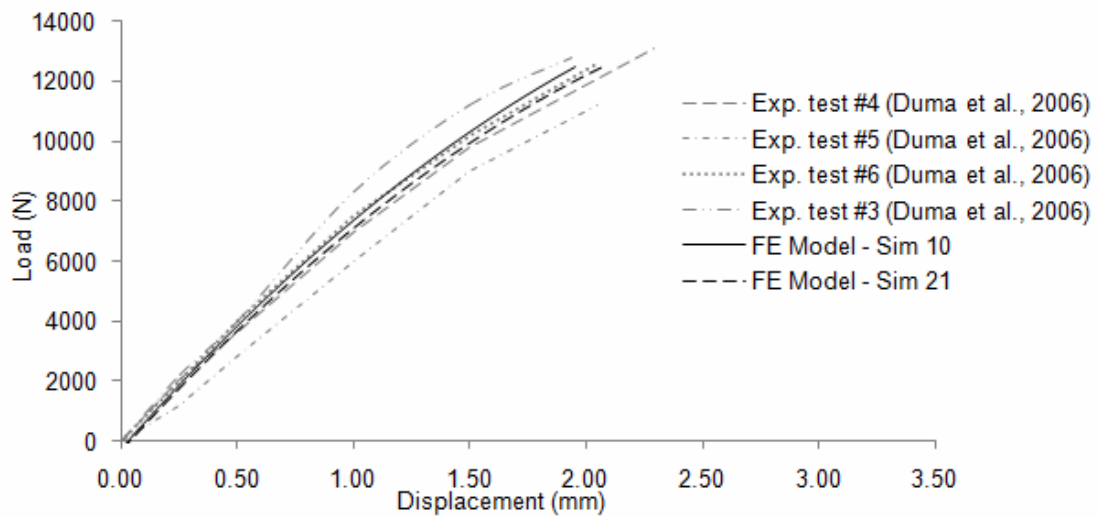


Intervertebral disc properties modelling (3/3)

Final solution : superimposition & intersection of Kcomp, Ffail & Dfail domain



Relevancy of solutions to experimentals data

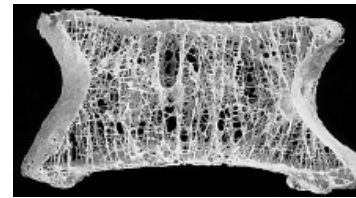
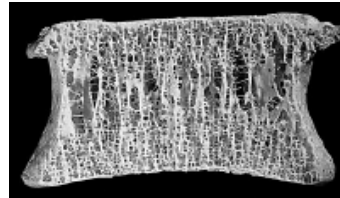


Bones properties (1/4)

Complexes structure – *many fracture & classifications*

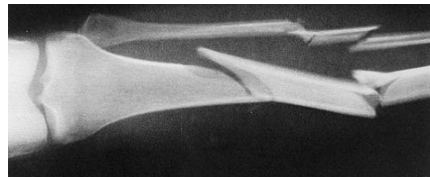
Some differences :

- Shape
- Composition (compact and spongy bone et os spongieux)
- Spatial distribution & organisation (ex: diaphysis & epiphysis)

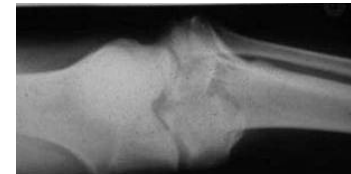


Bones injuries

Loaded under / *compression*
flexion
torsion



Comminuted spiral fracture



Proximal failure



Simple failure

Mechanical behaviour

Anisotropic (transverse isotropic) material

Heterogeneity & brittle behaviour

Elastoplastique dissymmetric behaviour,

Bones properties (2/4)

Long bones properties

3 point bending tests on long bones

Objectives :

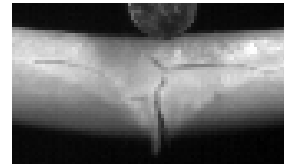
- Data for model validation
- Failure behaviour for long bones
- Variability {
 - âge, sexe*
 - orientation*
 - minéralisation*



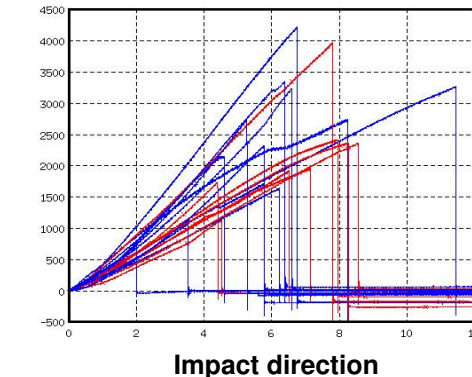
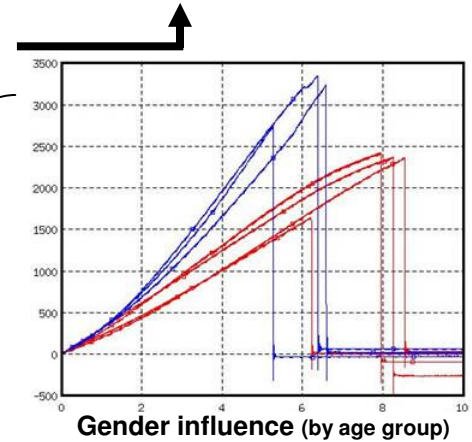
21 femur et 38 tibia tested

Results :

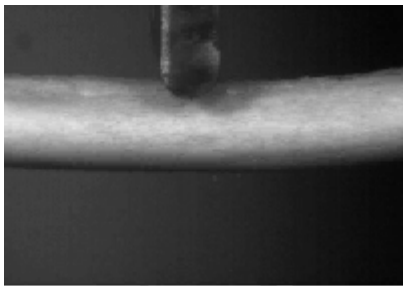
- An opening failure proces (which spend 2ms) :



- Age and gender, orientation influence on results

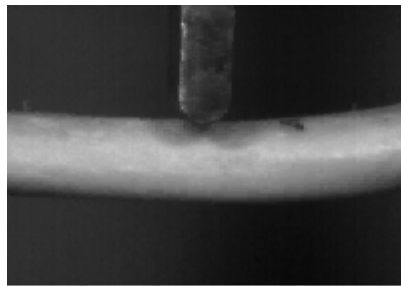


fracture simple oblique $\geq 30^\circ$



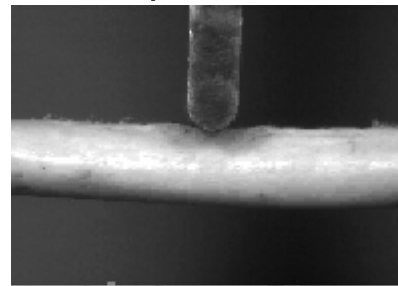
7/22/05 15:37:51 11450 5723,8[m \cdot s]
CAM profile_5 (2-row) (2000 Hz)

fracture à coin de flexion entier



22/07/05 14:08:22 12500 6248,6[m \cdot s]
CAM profile_5 (2-row) (2000 Hz)

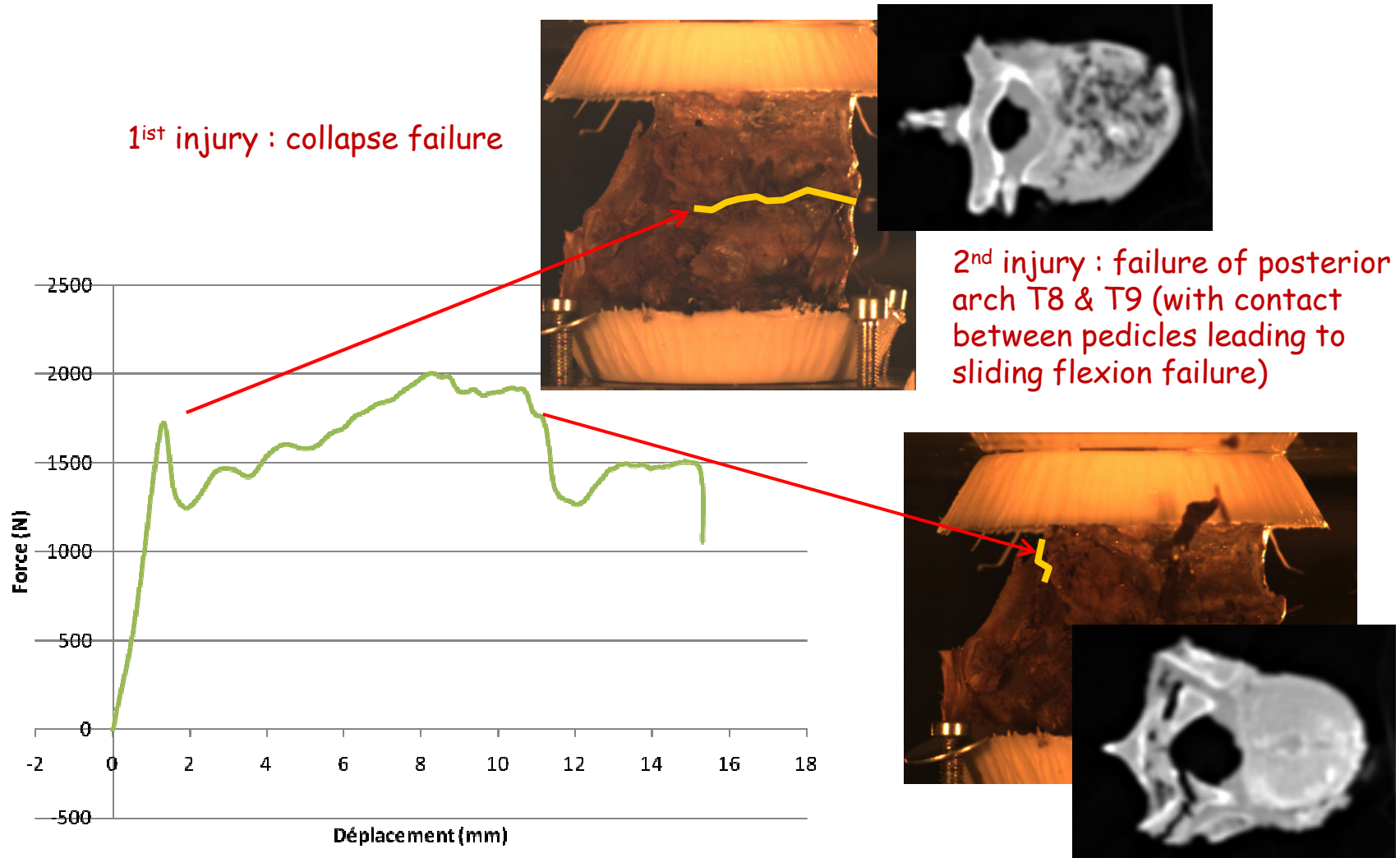
fracture simple transversale $< 30^\circ$



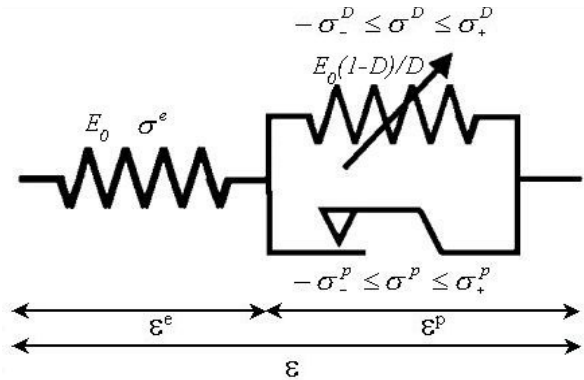
22/07/05 11:15:27 5000 2499,2[m \cdot s]
CAM profile_5 (2-row) (2000 Hz)

Spine : combine spongious and cortical bones structures

A multiple fracture level process with a gradation in injury severity



- "Elastoplastic" model with damage (Curnier, Garcia, Zysset)



Constitutive equations : $\sigma = E_0(\epsilon - \epsilon^p)$ $\sigma^p = E_0(\epsilon - \epsilon^p) - E_0 \frac{1-D}{D} \epsilon^p$

Damage law : $\dot{D} = \frac{\sigma_+^D \dot{\epsilon}^p}{E \left(\epsilon^p + \frac{\sigma_+^D}{E} \right)^2}$ $Y = \frac{1}{D^2} \frac{E_0}{2} \epsilon^{p2}$

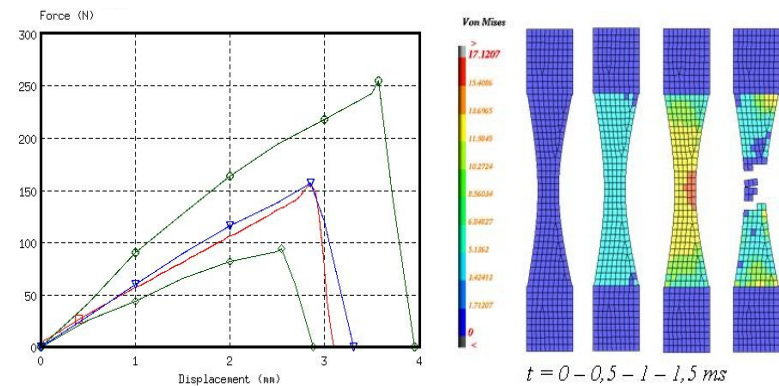
Failure : Energy criteria – Kill element method

A dissymétrique behaviour law

- Johnson Cook models also used

- Implementation in FE software as users laws

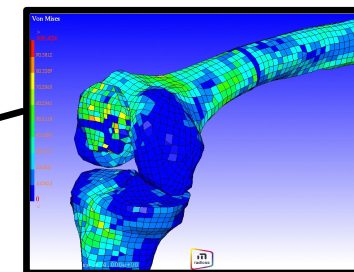
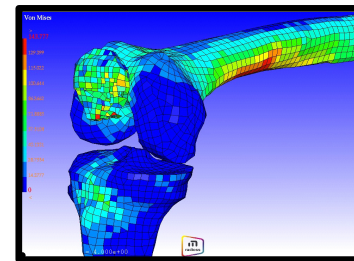
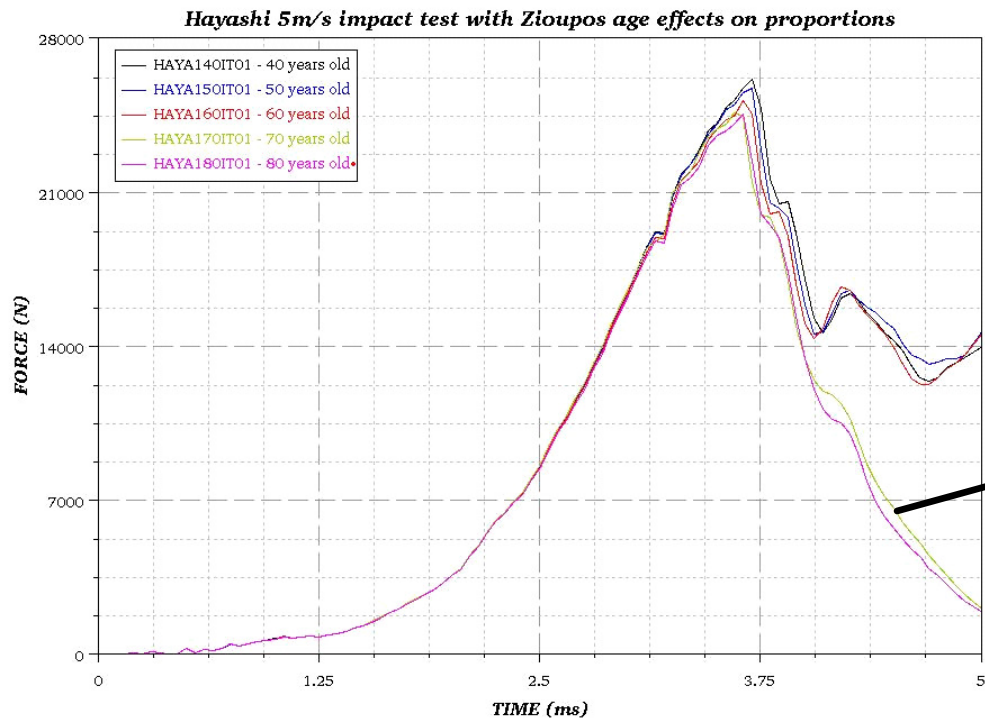
- Inverse analysis to identify model parameters



Implementation of human variability in bone structures (1/2)

Age effects

- Density
- Geometry (shap, thickness)
- Mechanical properties E , σ_{\max} , ϵ_{\max} , ...
- Amplified with impact velocity



Lower limb under frontal impact (car occupant impact)

Towards fully personalized model

Model geometry and properties obtained from calibrated CT scan

For $BMD_{QCT} < 0,06 \text{ mg/cm}^3$:

$$E(MPa) = 2980 * BMD_{QCT}^{1.05}$$

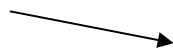
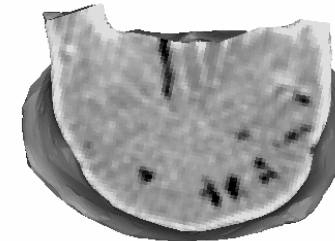
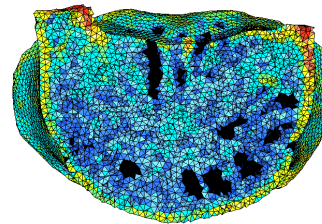
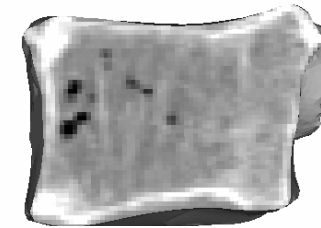
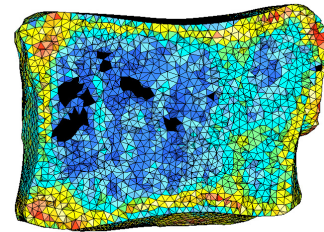
$$\sigma_y(MPa) = 37.4 * BMD_{QCT}^{1.39}$$

For $BMD_{QCT} > 0,06 \text{ mg/cm}^3$:

$$E(MPa) = -34.7 + 3230 * BMD_{QCT}$$

$$\sigma_y(MPa) = -0.750 + 24.9 * BMD_{QCT}$$

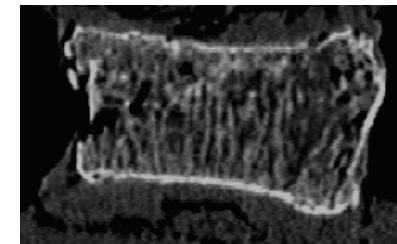
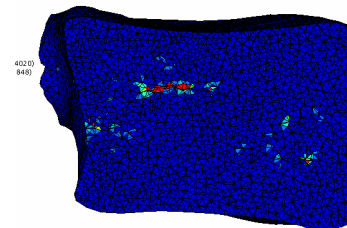
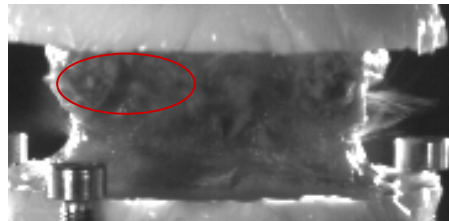
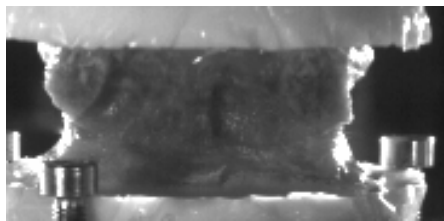
$$\sigma_{\max}(MPa) = 1.2 * \sigma_y$$



Relationship valid for Quasi-static loading

Corrective coefficient to be implemented for dynamic loadings

Validated with experimental compression tests (1m/s)



II. On human body modeling

II. On Human body modeling

Which models for which applications ?

Human body model for dynamic loadings & constraints to explicit FE platforms

Simplified models

Particularities :

Rigid Body in FE simulations
Tuned validations

Advantage :

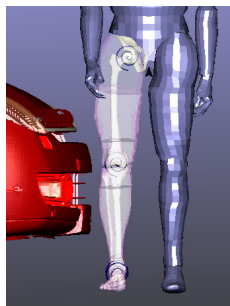
Calculation time

Drawbacks :

Model validity and biofidelity

Applications :

Optimisation
Globale vision



LLMS Hybride

Robusts deformable models

Particularities :

Description anatomique
Structures ayant une contribution mécanique

Advantage :

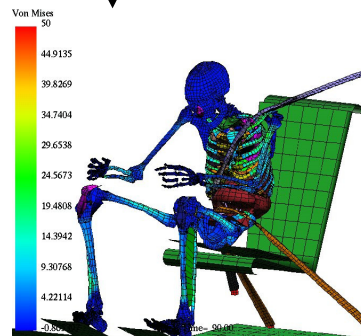
Robustesse % calculation time

Drawbacks :

Sensitivity to model

Applications :

Global injury mechanisms understanding
Safety systems evaluation



Modèle HUMOS

Detailed models

Particularities :

Complete anatomical description

Advantages :

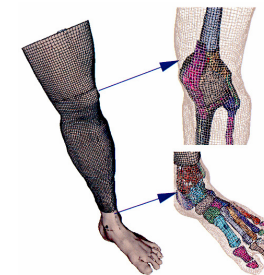
Results quality

Drawbacks :

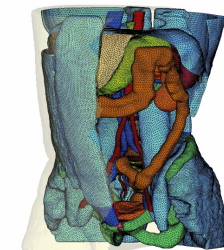
Calculation time

Applications :

Accurated local analysis
Enlarged applications to crash



Modèle LLMS



Modèle MELBA

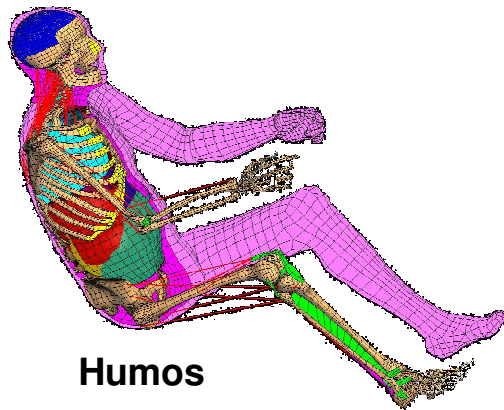
II. On Human body modeling

From medical data to modelling

- An accurate geometrical description to investigate structure effects

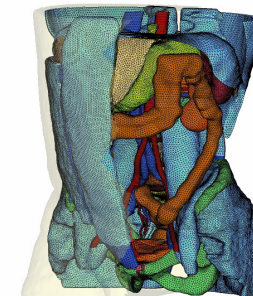
- Structures with a mechanical contribution
- Structures with physiological functions

- Coupled / Compatibles model Multi-level analysis of injuries

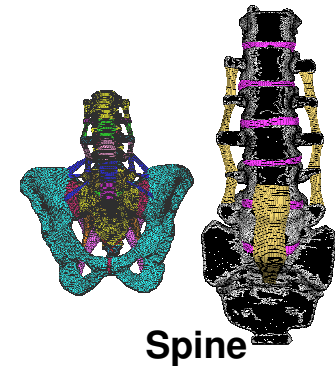


1997: 50 000 elements for a body model

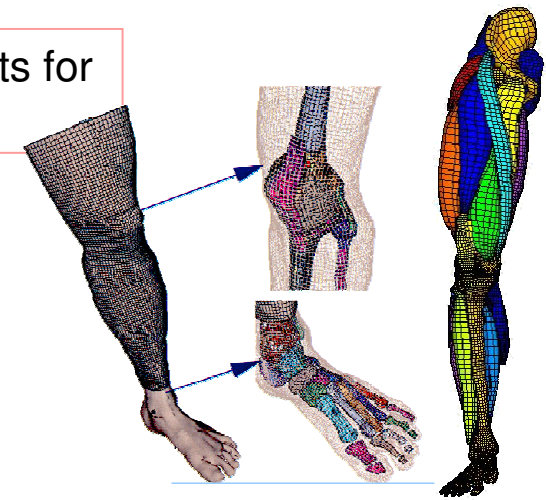
2009: 3 000 000 elements for the abdomen



Trunk
Abdomen and plevis



Spine

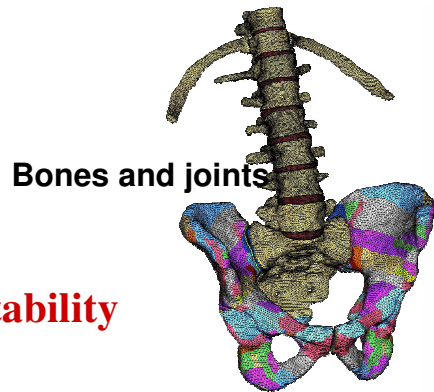


Lower limb

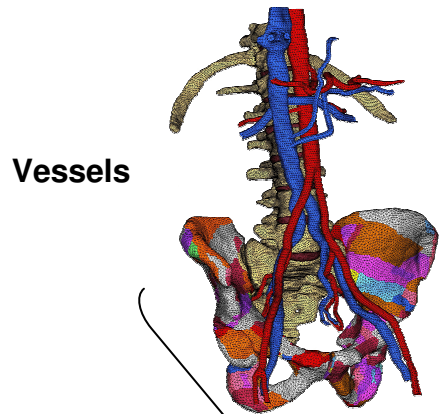
II. On Human body modeling

The abdominal segment

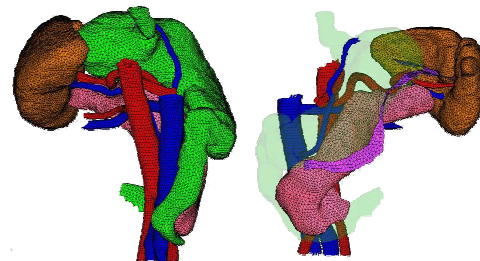
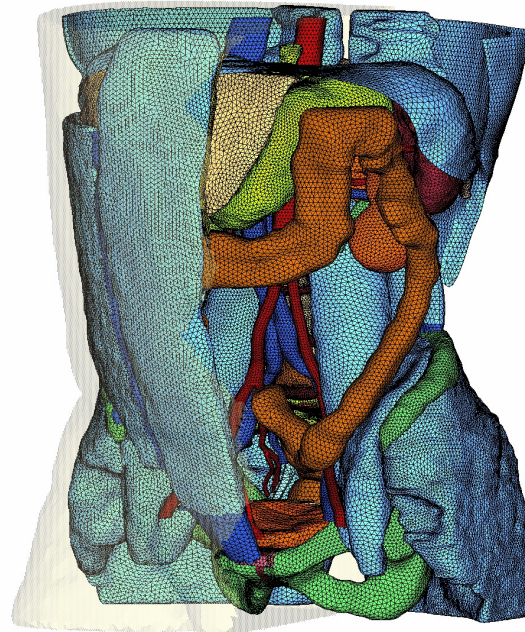
From mechanical contribution to injury indication



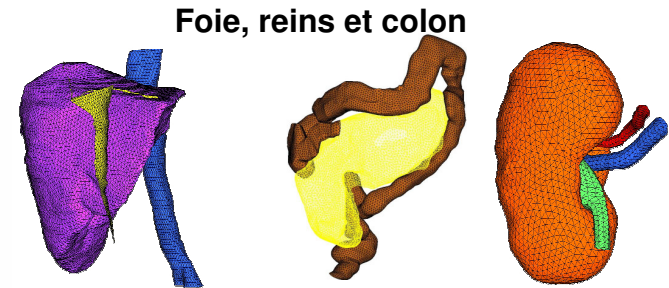
Stability



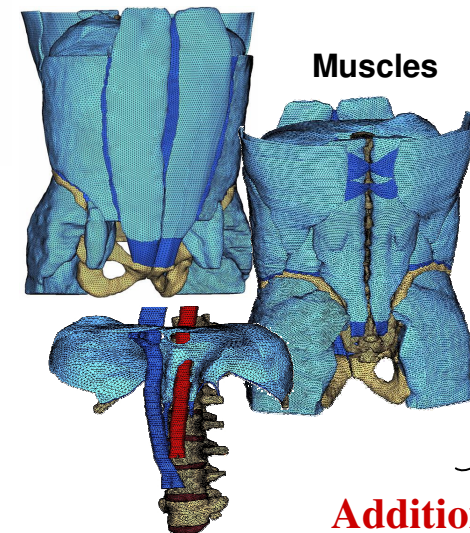
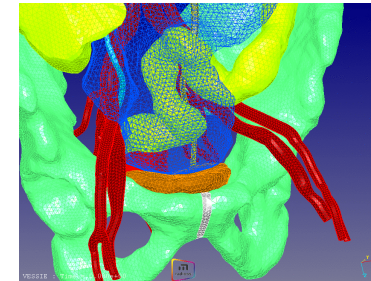
Organs attachment



estomac-duodéum-pancréas-rate



La vessie



Additional strength
Modulate pressure...

II. On Human body modeling

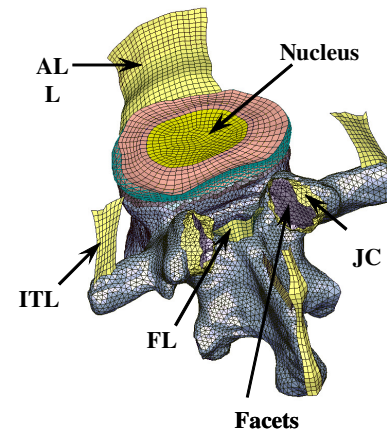
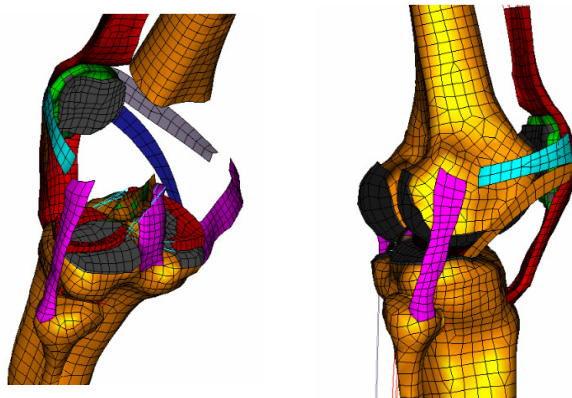
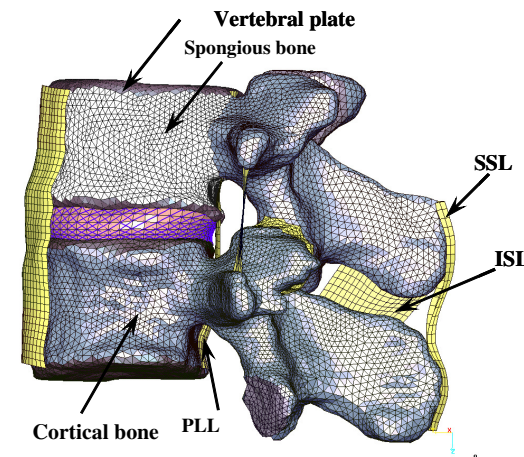
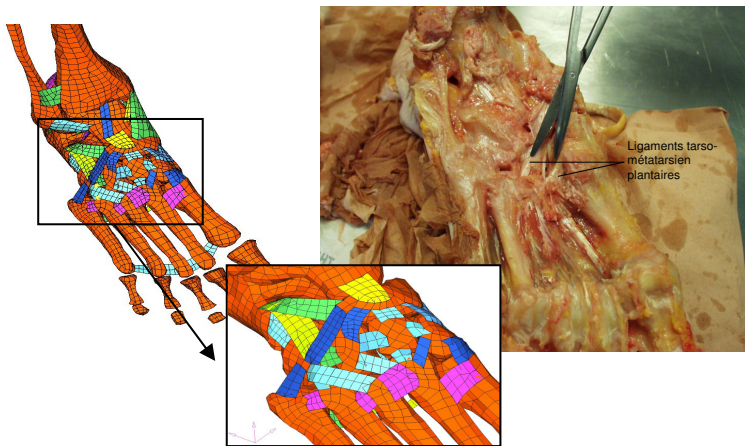
The challenge of joint modeling

Joint modelling combine :

Contact conditions (hard-hard, hard-soft tissues)

Mobilities (physiological kinematics)

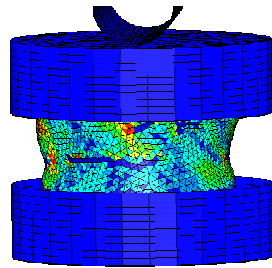
Mechanical (& numerical) stability



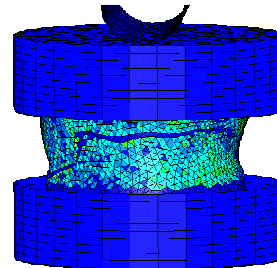
II. On Human body modeling

Geometrical and physical properties

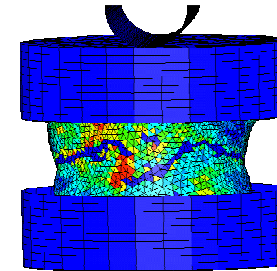
On the variability of properties distributions



Homogenous properties,

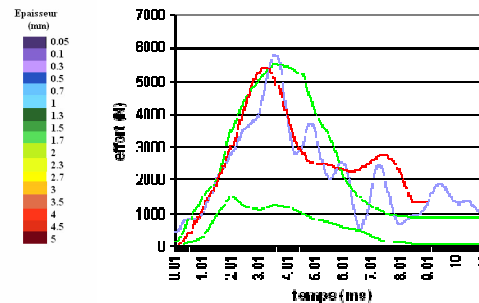
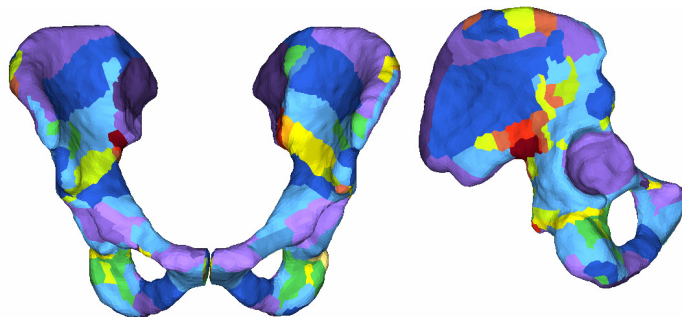


heterogenous random properties,



Full personalisation

Integration of thickness distributions

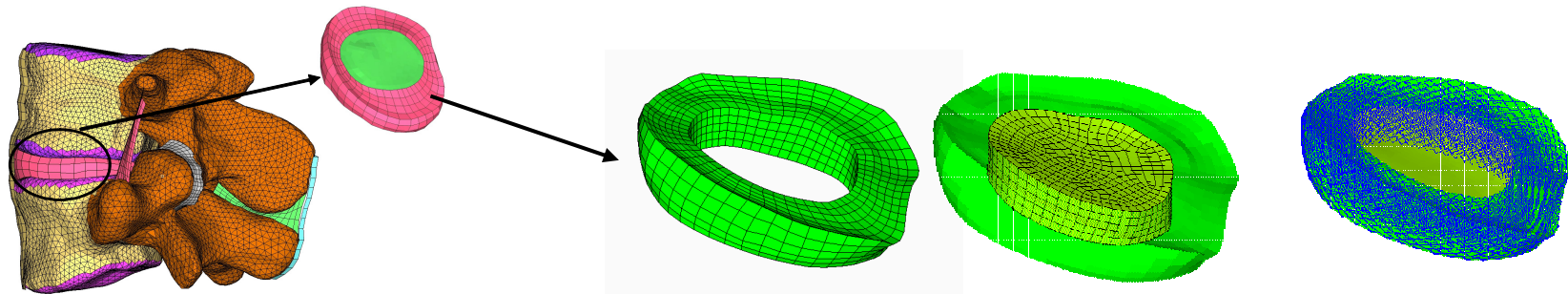


Limitation of vibrations with geometrical thickness cortical bone thickness distribution (side impact for pelvis)

II. On Human body modeling

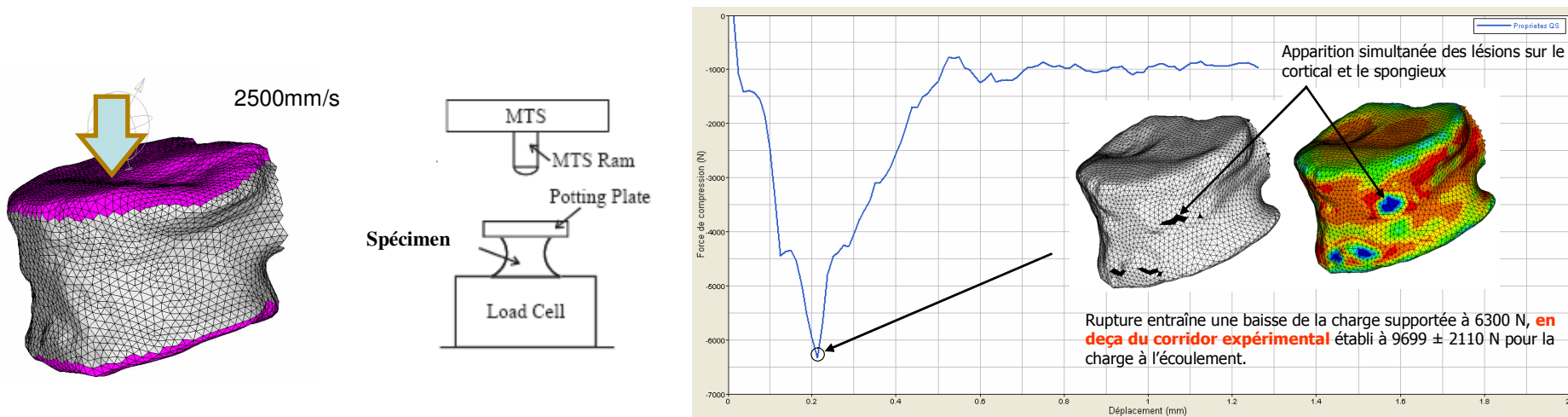
Geometrical and physical properties

Links between structure specificities modelling choices



Spine functional unit : Viscoelasticity – Incompressibility – Fibrous reinforcements

Geometrical non linearity : an indicator for potential failure



III Applications to virtual trauma

About vulnerable road users

- Pedestrian & lower limb injuries
- Spine trauma : Motorcyclists

III. Applications to virtual trauma

Aims and methodology with virtual trauma

Injury chronology analysis : { *Injury mechanisms*
Injury criteria

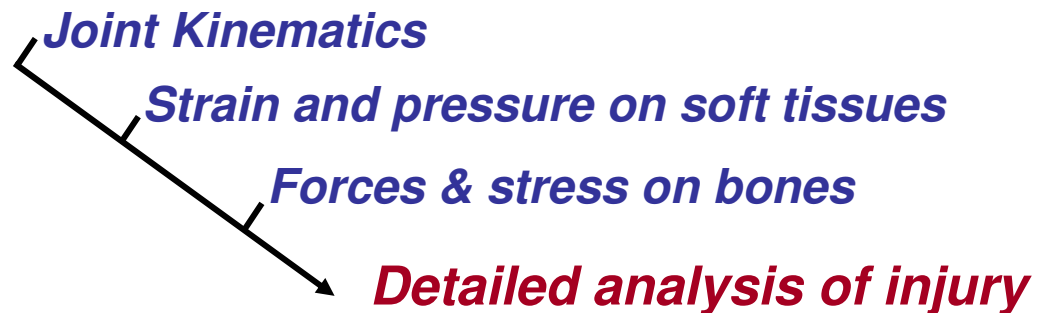
According to validated models



/ Investigate new impact conditions

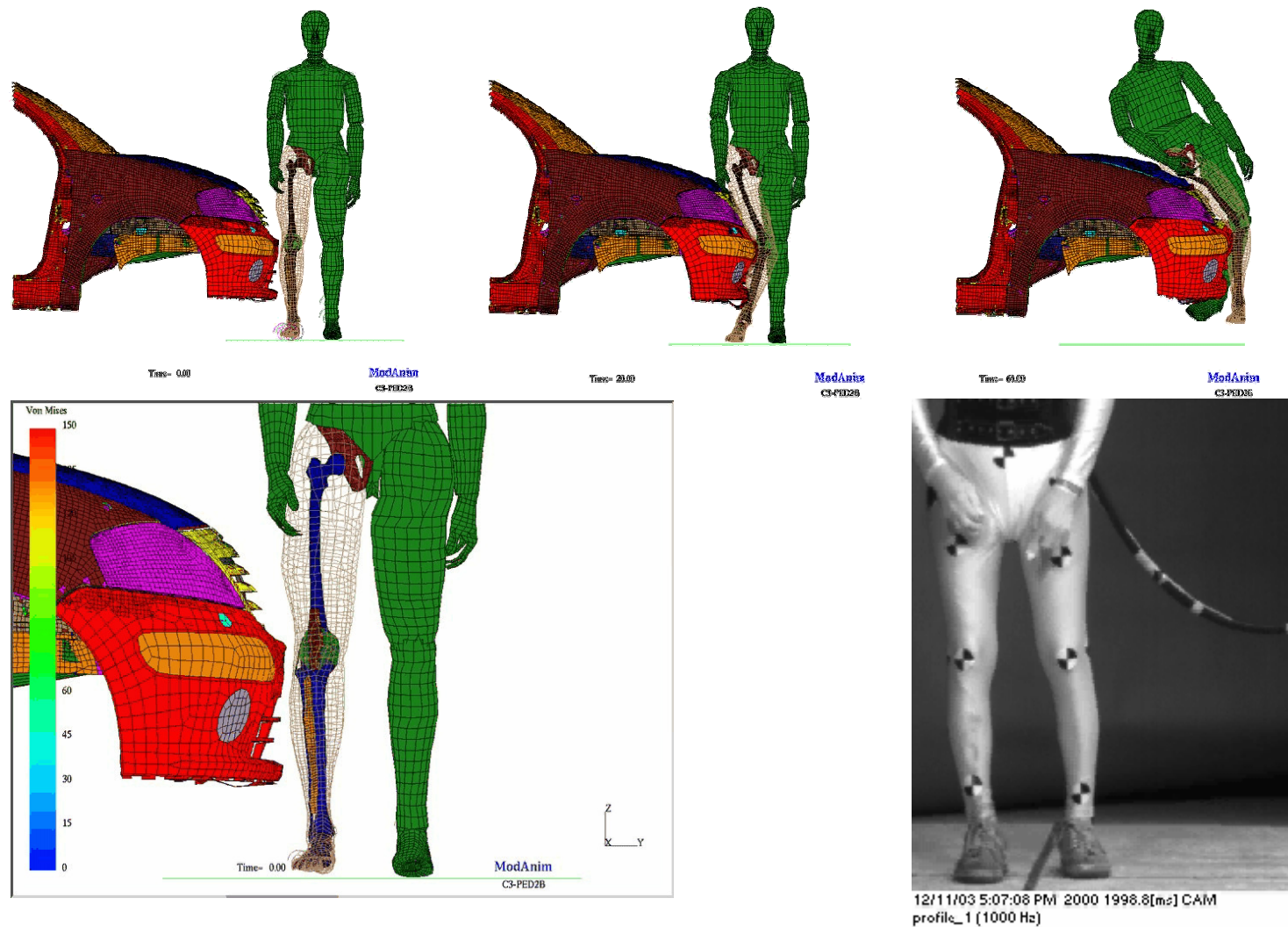
/ Obtain data which can not be recorded during experiments

Methodology : *A combined clinical and mechanical analysis*



III. Applications to virtual trauma

On pedestrian lower limb safety

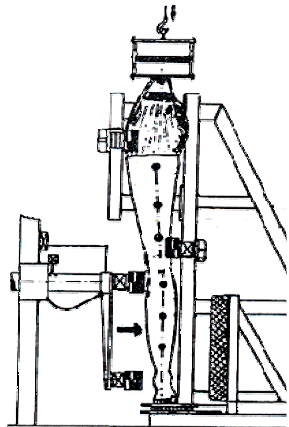


Lateral shearing and bending govern knee injuries

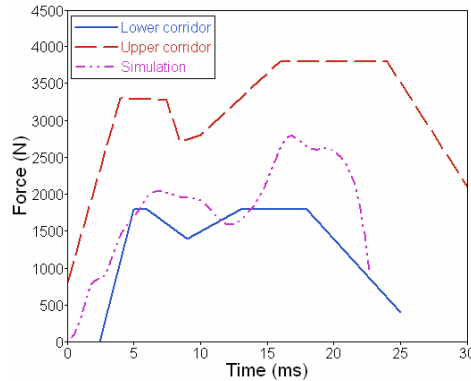
III. Applications to virtual trauma

On pedestrian lower limb safety

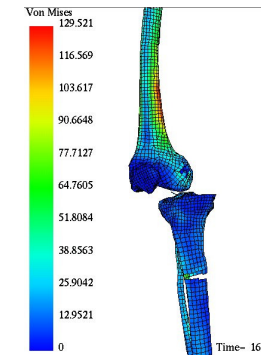
Case of pure shearing



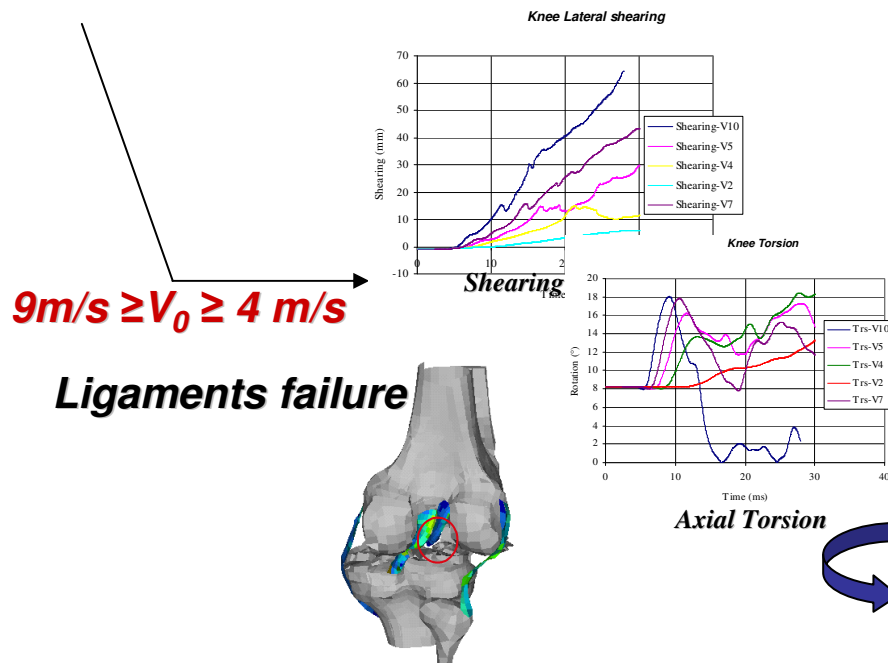
Kajzer (5.55m/s)



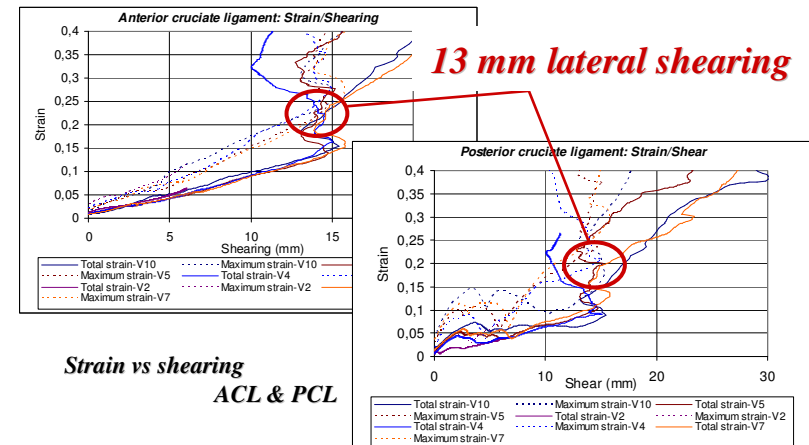
$$V_0 \geq 10 \text{ m/s}$$



Tibia fracture



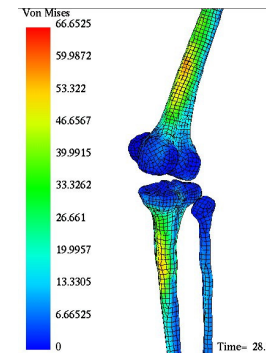
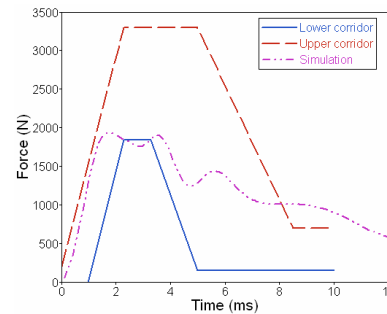
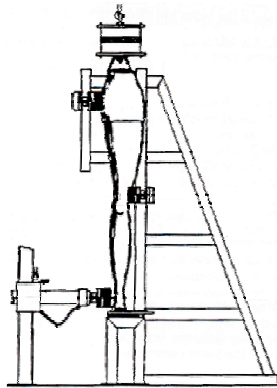
Relationship between ligaments strain and global shearing



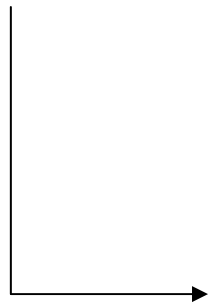
III. Applications to virtual trauma

On pedestrian lower limb safety

Case of pure bending

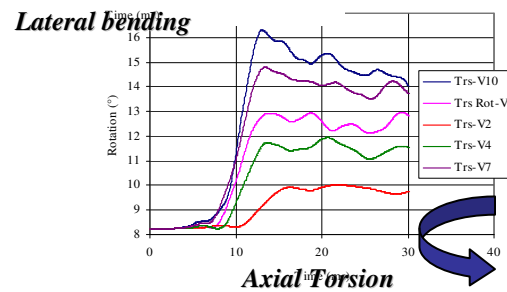
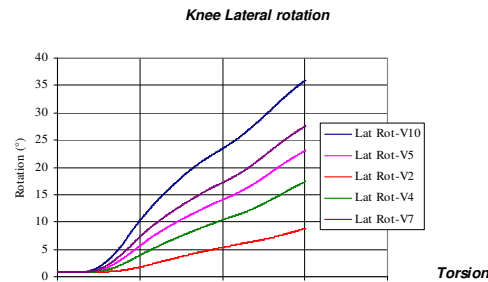


Kajzer (5.55m/s):

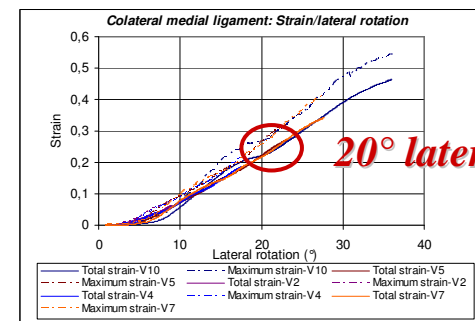


$10\text{m/s} \geq V_0 \geq 4\text{ m/s}$

Ligaments failure



Relationship between ligaments strain and global bending

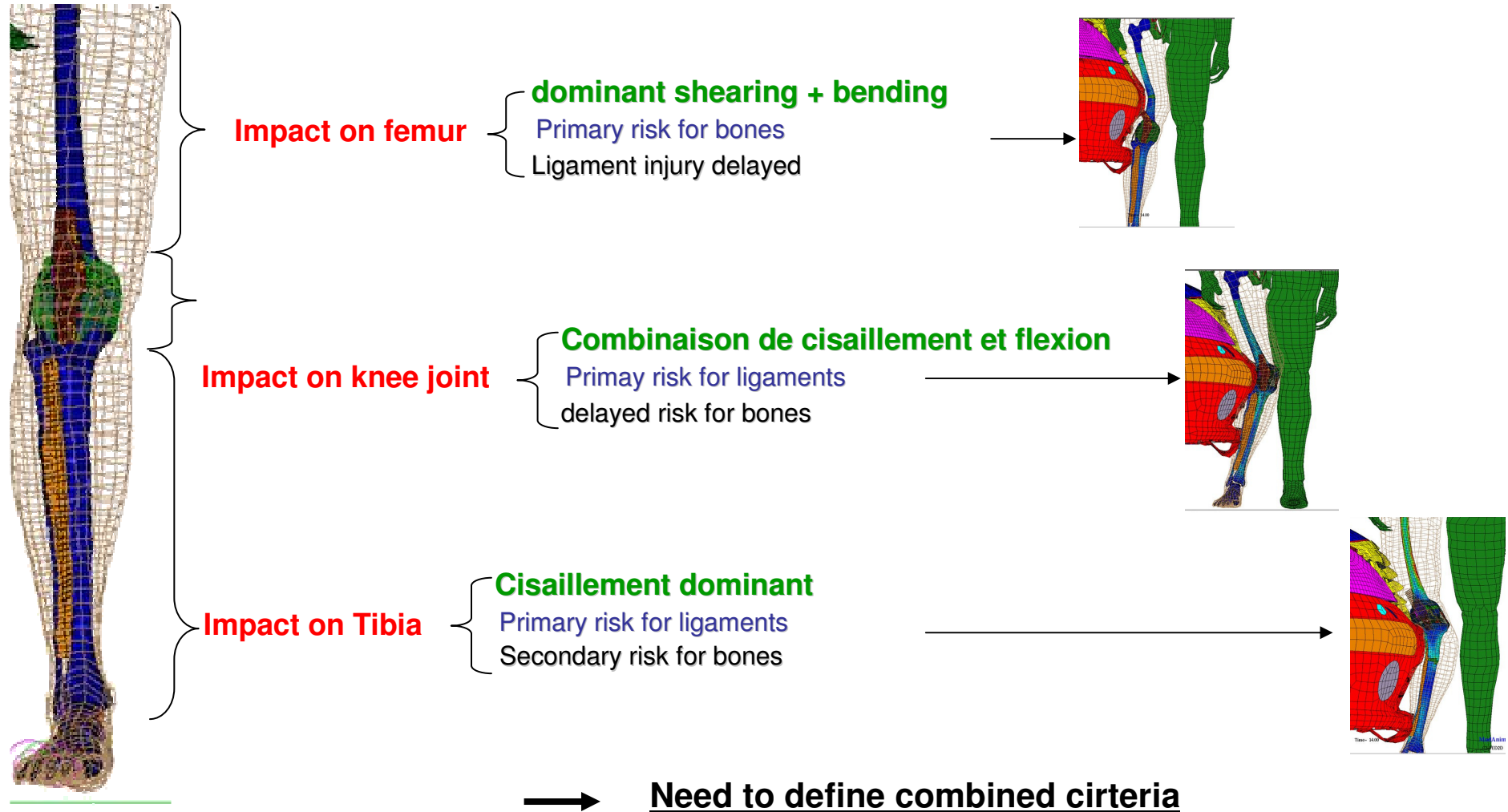


Strain vs lateral bending on MCL

20° lateral bending injury criteria

III. Applications to virtual trauma

On pedestrian lower limb safety

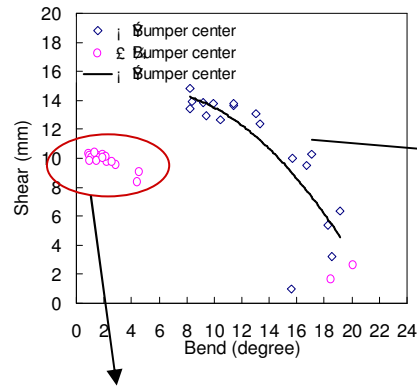
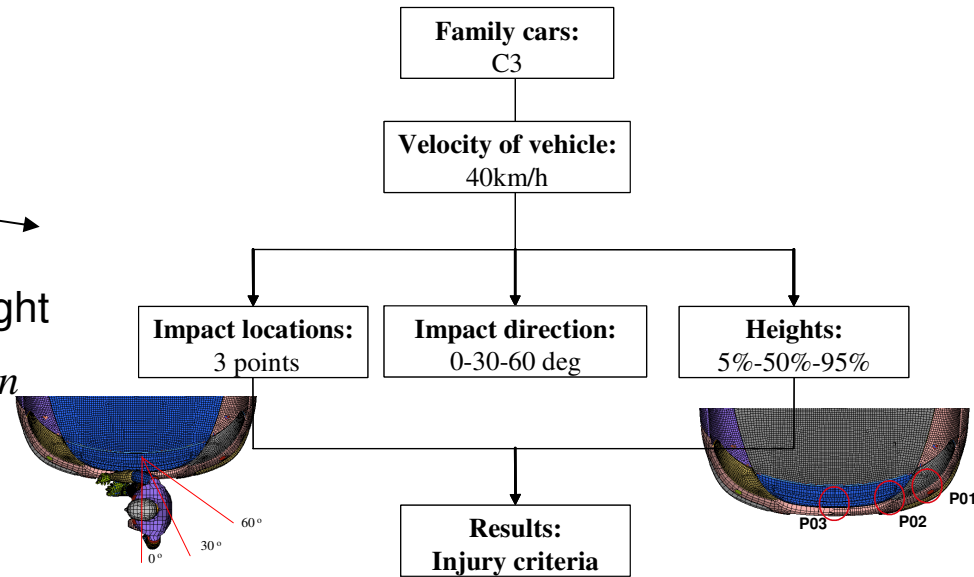


III. Applications to virtual trauma

On pedestrian lower limb safety

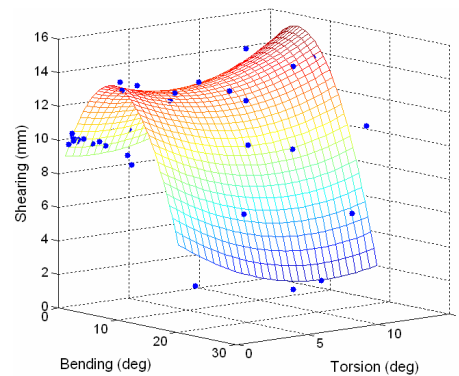
A two step sensitivity analysis

- 1: 27 runs on impact variability
- 2: 36 additional runs focusing on impact height
12 height levels from 5% to 95% pedestrian



A shearing criteria for femur and tibia impact

An injury risk surface for knee joint impact combining shearing, bending & torsion



Injury function	
$d_s = 7.992 + 1.313\alpha_b - 0.111\beta_t - 0.027\alpha_b\beta_t - 0.073\alpha_b^2 + 0.031\beta_t^2$	
R ²	
69%	

Shearing- d_s
 Bending- α_b
 Torsion- β_t

III. Applications to virtual trauma

On Spine trauma current investigations

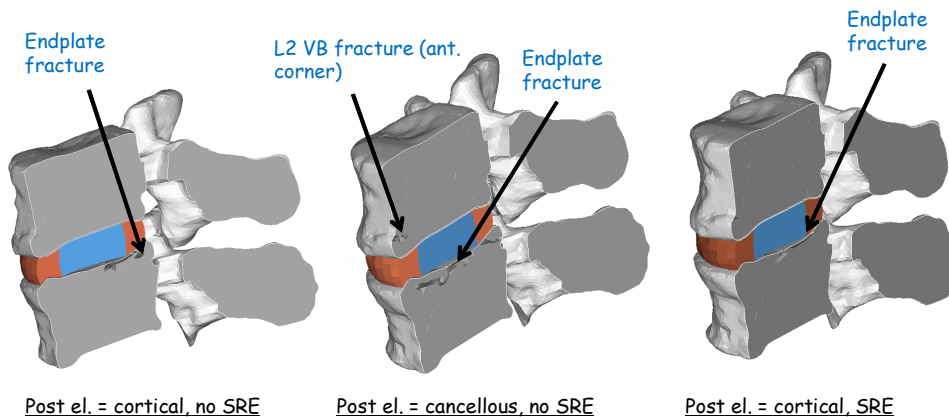
Spine fracture with instability



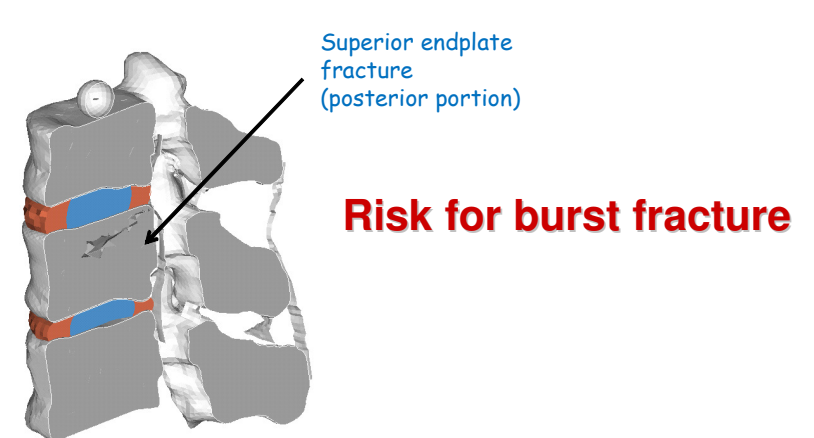
→ Flexion - Extension
Axial compression

- Vulnerability changes according to spine location

Endplate bone fracture on L2-L3



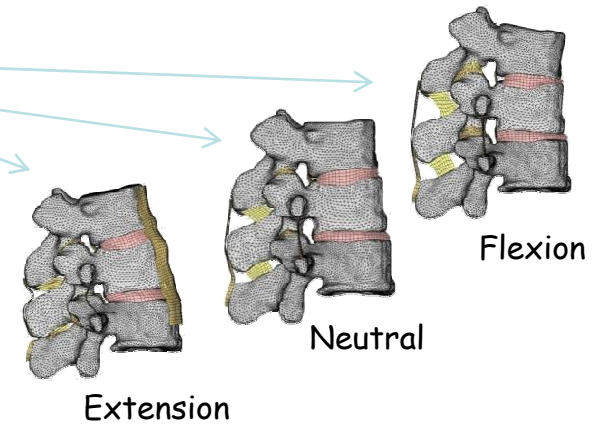
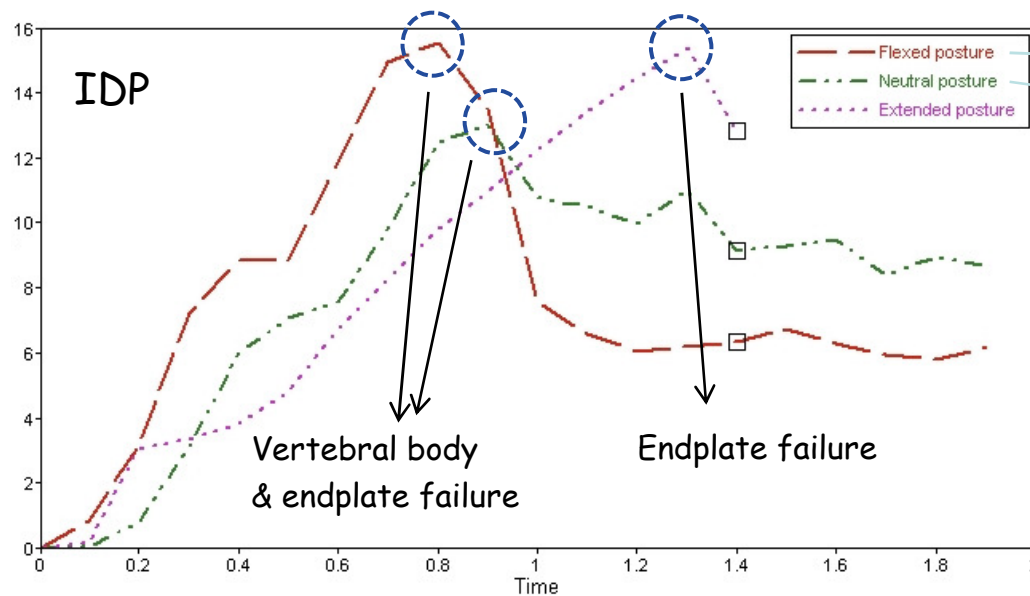
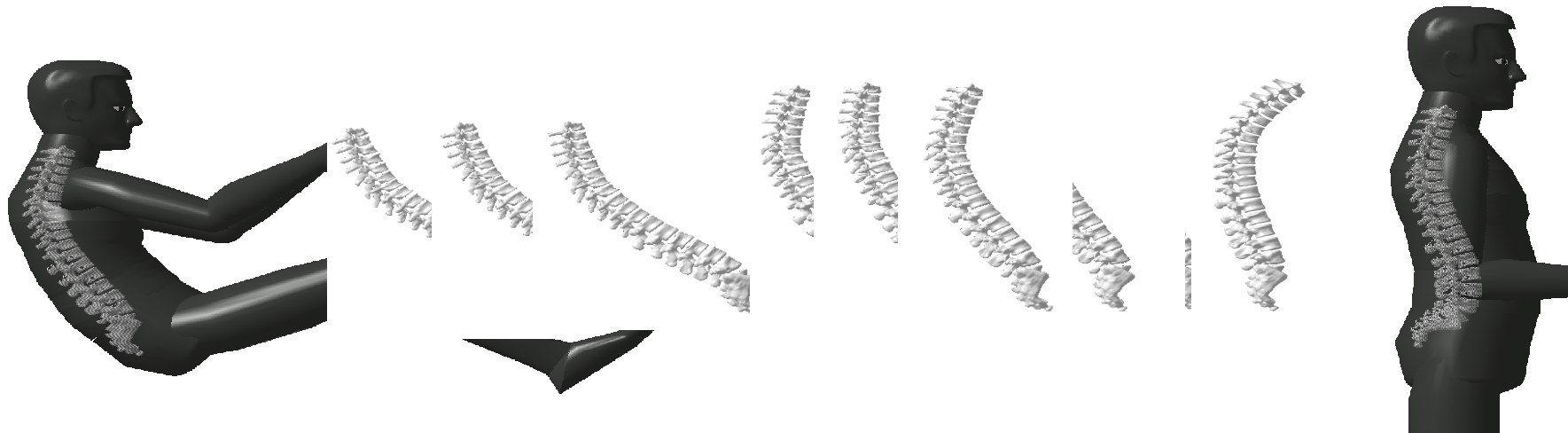
Endplate bone fracture on T12-L5



III. Applications to virtual trauma

On Spine trauma current investigations

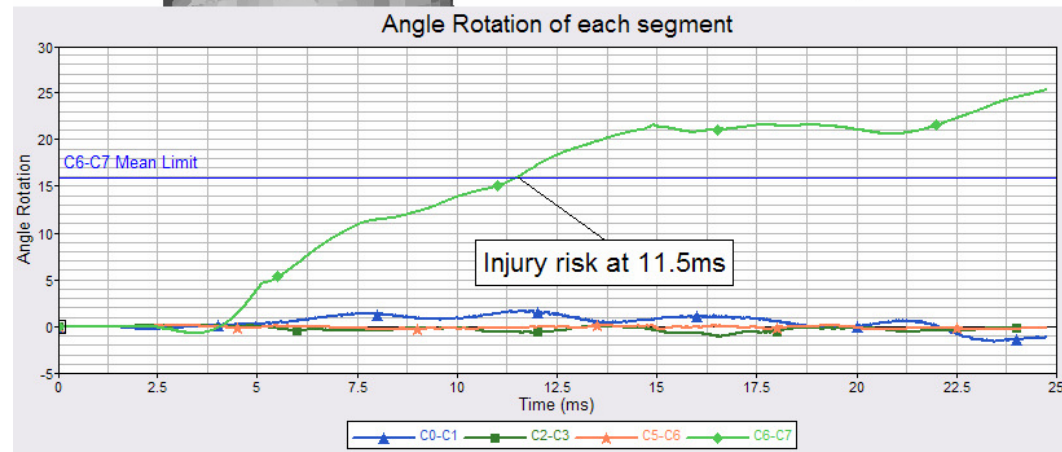
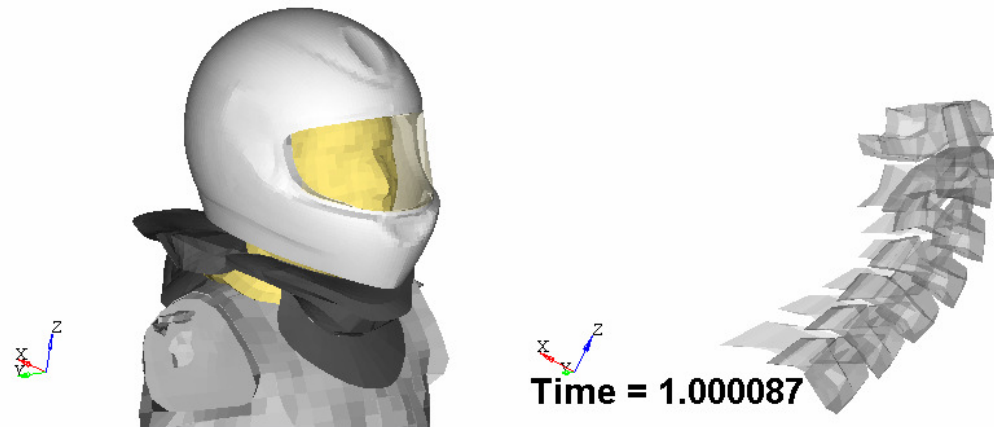
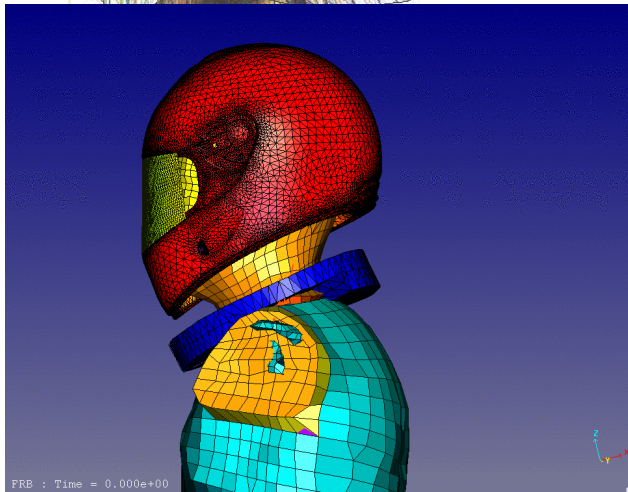
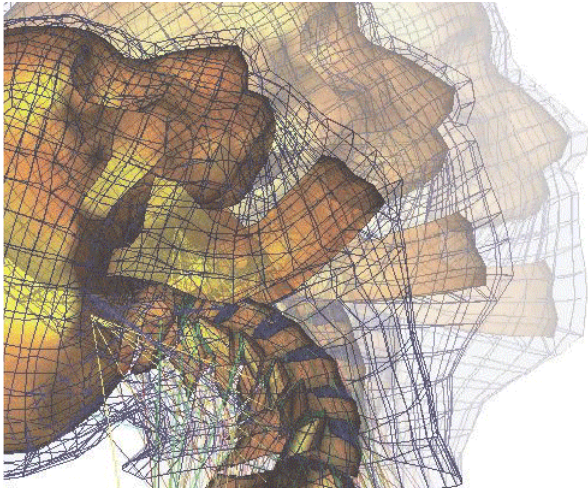
- Vulnerability changes according to spine curvature



III. Applications to virtual trauma

On Spine trauma current investigations

- From cervical spine vulnerability to safety systems evaluation



Discussion – Conclusion on biological tissues properties

Hard tissues

Fibrous tissues

Soft Tissues

- **Dedicated experiments for tissues identification** { Traction
Compression
- **Simple behaviour laws :** | The main physical properties
Dynamic loadings
- **Use recordable parameters in models :** | Closed to experiments
Introduction of human variability
- **A numerical environment**

Discussion – Conclusion on human modelling

The choice to define detailed FE models

On modeling tasks : des exigences et des questions

- Meshing tasks** { Needs to optimise choice of elements
Discontinuous mesh
- Modelling** { All tissues should be investigated up to failure
Human variability from ages, sexe, ... – also from modelling choices
Which interactions for organs, ...
- Validation** { A multi-level analysis

On Virtual trauma

Work on relationship between mechanical understanding and clinical features

A numerical model is tool, not a true



**Which validity ?
Which analysis ?**

Remerciements

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